

**A METHOD OF APPLYING A TUBE MEMBER IN A STATOR SLOT
IN A ROTATING ELECTRICAL MACHINE**

Technical field

5 The present invention relates to rotating electric machines such as syn-
chronous machines. It also relates to double-fed machines, applications in asyn-
chronous static current converter cascades, external pole machines and synchro-
nous flux machines, as well as to alternating current machines intended primarily
as generators in a power station for generating electric power. The invention par-
10 ticularly relates to the stator in such machines and a method for fixing the wind-
ings, as well as cooling the stator teeth and the insulated electric conductor con-
stituting the stator winding.

Background art

15 Similar machines have conventionally been designed for voltages in the
range 15-30 kV, and 30 kV has normally been considered to be an upper limit.
This generally means that a generator must be connected to the power network
via a transformer which steps up the voltage to the level of the power network,
which is in the range of approximately 130-400 kV. The present invention is in-
20 tended primarily for use with high voltages. High voltages shall be understood
here to mean voltages in excess of 10 kV. A typical operating range for the ma-
chine according to the invention may be voltages from 36 kV up to 800 kV. The
invention is secondarily intended for use in the stated technical area at voltages
below 36 kV.

25 Two different air-cooled systems exist for conventional cooling: radial
cooling where the air passes the rotor through the hub and radial channels in the
rotor, and axial cooling where the air is blown into the pole gaps by axial fans. The
stator is divided into radial air ducts created by means of (often straight) spacers
that are welded in place. Due to the poor thermal conductivity axially through the
30 stator laminations the air ducts must be frequently repeated. The drawback with
air-cooling is that the ventilation losses are considerable and that, because of the
ventilation ducts, the stator becomes longer. Furthermore, particularly with said

high-voltage generators with long teeth, the ventilation ducts may also weaken the structure mechanically.

Axial liquid cooling, e.g. water-cooling, by means of cooling tubes, e.g. of metal, in the stator yoke has been known for some time. One drawback is that eddy currents are induced in metal tubes if they are present in a magnetic flux varying with time, thus leading to certain power losses when used in an electric machine.

Object of the invention

The object of the present invention is to provide a method for mounting a cooling tube in a cooling tube channel, and also a rotating electric machine comprising cooling tubes mounted using this method in conjunction with direct cooling of the stator and particularly the stator teeth in such a machine.

Another object of the invention is to eliminate ventilation ducts, thereby resulting in shorter and stronger stators, at the same time as ensuring that the magnetic flux in the stator teeth is disturbed as little as possible by said cooling. The object is also to achieve a higher degree of efficiency.

A further object of the invention is to achieve a steady fixing of the cables in the stator slots by means of these cooling tubes.

Summary of the invention

The above-mentioned object is achieved by the method and the arrangement in accordance with the invention having the features defined in the appended claims.

By using high-voltage insulated electric conductors with solid insulation similar to that used in cables for transmitting electric power (e.g. XLPE-cables) the voltage of the machine can be increased to such levels that it can be connected directly to the power network without an intermediate transformer. The conventional transformer can thus be eliminated. The concept generally requires the slots in which the cables are placed in the stator to be deeper than with conventional technology (thicker insulation due to higher voltage and more turns in the winding). This means that the distribution of losses differs from that in a conventional

machine, which in turn entails new problems in cooling the stator, for instance, and particularly the stator teeth.

The insulated conductor or high-voltage cable used in the present invention is flexible and is of the type described in more detail in WO 97/45919 and
5 WO 97/45847. The insulated conductor or cable is described further in WO 97/45918, WO 97/45930 and WO 97/45931.

Thus, in the device in accordance with the invention the windings are preferably of a type corresponding to cables having solid, extruded insulation, like those currently used for power distribution, such as XLPE-cables or cables with
10 EPR-insulation. Such a cable comprises an inner conductor composed of one or more strand parts, an inner semiconducting layer surrounding the conductor, a solid insulating layer surrounding this and an outer semiconducting layer surrounding the insulating layer. Such cables are flexible, which is an important property in this context since the technology for the device according to the inven-
15 tion is based primarily on winding systems in which the winding is formed from conductors which are bent during assembly. The flexibility of a XLPE-cable normally corresponds to a radius of curvature of approximately 20 cm for a cable 30 mm in diameter, and a radius of curvature of approximately 65 cm for a cable 80 mm in diameter. In the present application the term "flexible" is used to indicate
20 that the winding is flexible down to a radius of curvature in the order of four times the cable diameter, preferably eight to twelve times the cable diameter.

The winding should be constructed to retain its properties even when it is bent and when it is subjected to thermal or mechanical stress during operation. It is vital that the layers retain their adhesion to each other in this context. The material properties of the layers are decisive here, particularly their elasticity and rela-
25 tive coefficients of thermal expansion. In a XLPE-cable, for instance, the insulating layer consists of cross-linked, low-density polyethylene, and the semiconducting layers consist of polyethylene with soot and metal particles mixed in. Changes in volume as a result of temperature fluctuations are completely absorbed as changes in radius in the cable and, thanks to the comparatively slight
30 difference between the coefficients of thermal expansion in the layers in relation

to the elasticity of these materials, the radial expansion can take place without the adhesion between the layers being lost.

The material combinations stated above should be considered only as examples. Other combinations fulfilling the conditions specified and also the condition of being semiconducting, i.e. having a resistivity within the range of 10^{-1} - 10^6 ohm-cm, e.g. 1-500 ohm-cm, or 10-200 ohm-cm, naturally also fall within the scope of the invention.

The inner and outer semiconducting layers may be of the same basic material but with particles of conducting material such as soot or metal powder mixed in.

The mechanical properties of these materials, particularly their coefficients of thermal expansion, are affected relatively little by whether soot or metal powder is mixed in or not - at least in the proportions required to achieve the conductivity necessary according to the invention. The insulating layer and the semiconducting layers thus have substantially the same coefficients of thermal expansion.

Ethylene-vinyl-acetate copolymer/nitrile rubber, butylmp polyethylene, ethylene-acrylate-copolymers and ethylene-ethyl-acrylate copolymers may also constitute suitable polymers for the semiconducting layers.

Even when different types of material are used as base in the various layers, it is desirable for their coefficients of thermal expansion to be substantially the same. This is the case with the combination of the materials listed above.

The materials listed above have relatively good elasticity, with an E-modulus of $E < 500$ MPa, preferably < 200 MPa. The elasticity is sufficient for any minor differences between the coefficients of thermal expansion for the materials in the layers to be absorbed in the radial direction of the elasticity so that no cracks or other damage appear and so that the layers are not released from each other. The material in the layers is elastic, and the adhesion between the layers is at least of the same magnitude as in the weakest of the materials.

The conductivity of the two semiconducting layers is sufficient to substantially equalize the potential along each layer. The conductivity of the outer semiconducting layer is sufficiently large to contain the electrical field in the cable, but

at the same time sufficiently small not to give rise to significant losses due to currents induced in the longitudinal direction of the layer.

Thus, each of the two semiconducting layers essentially constitutes one equipotential surface, and the winding composed of these layers will substantially
5 enclose the electrical field within it.

There is, of course, nothing to prevent one or more additional semiconducting layers being arranged in the insulating layer.

The invention relates to a method for fixing the cable in a high-voltage generator by means of a pre-shaped triangular tube of XLPE that during operation is
10 also used for cooling the windings and the tooth section of the stator core. At the assembly, the pre-shaped tube is inserted into the triangular space between cables and tooth. The shape of the tube should provide enough clearance to permit easy insertion of the tube. When the tube is in place, it is heated to a temperature of 125-130°C at which it may be shaped. Moreover, an overpressure is applied to
15 the inside of the tube in order to press the tube against the cables and the slot wall. Both heating and pressurising of the tube are achieved by heating and pressurising a pressure medium, causing the tube to soften and expand, whereby its outer periphery assumes a shape fitting against cables and slot wall. While retaining the overpressure, the tube is then cooled by exchanging the warm pressure medium against a cold pressure medium, e.g. cold water, which fills the expanded tube and causes it to solidify and permanently assume this expanded
20 shape. The tube will now act as an elastic element, absorbing the thermal expansion of the cables during operation. The tube is also used as a cooling tube during operation, the overpressure of the cooling medium providing a steadying pressure on the cables. This pressure against cables and the slot wall improves the heat
25 transfer as well. The tubes are placed against one of the slot walls in every or every other cable interspace.

The invention also relates to a rotating electric machine provided with cooling tubes/fixing means mounted by this method.

30 The machine comprises axially running cooling tubes made of a dielectric material, e.g. a polymer, and drawn through the triangular cable interspaces in the stator teeth. The tubes are expanded in the interspaces so that good heat transfer

occurs when coolant is circulated in the tubes. The tubes run in the stator yoke and in the stator teeth along the entire axial length of the stator and, if necessary, they can be spliced in the stator teeth.

Polymer cooling tubes are non-conducting and the risk of short-circuiting is therefore eliminated, nor can eddy currents occur in them. Polymer cooling tubes can also be bent cold and drawn through several cooling tube channels without splicing, which is a great advantage.

Polymer cooling tubes can be produced from many materials, such as polyethylene, polypropene, polybutene, polyvinylidene fluoride, polytetrafluoroethylene, as well as filled and reinforced elastomers. Of these materials, polyethylene with high density, HDPE, is preferred since its thermal conductivity increases with increased density. If the polyethylene is cross-linked, which can be achieved by splitting a peroxide, silane cross-linking or radiation patterning, its ability to withstand pressure at increased temperature is enhanced, at the same time as the risk of voltage corrosion disappears. Cross-linked polyethylene, e.g. XLPE tubing from Wirsbo bruks AB, is used, for instance, for water pipes.

In a method and a device in accordance with the invention, the windings are preferably of a type corresponding to cables having solid, extruded insulation, like those currently used for power distribution, such as XLPE-cables or cables with EPR-insulation. Such a cable comprises an inner conductor composed of one or more strand parts, an inner semiconducting layer surrounding the conductor, a solid insulating layer surrounding this and an outer semiconducting layer surrounding the insulating layer. Such cables are flexible, which is an important property in this context since the technology for the device according to the invention is based primarily on winding systems in which the winding is drawn back and forth in a plurality of turns, i.e. without being spliced at the coil ends as required when the winding in the core consists of rigid conductors. The flexibility of a XLPE-cable normally corresponds to a radius of curvature of approximately 20 cm for a cable 30 mm in diameter, and a radius of curvature of approximately 65 cm for a cable 80 mm in diameter. In the present application the term "flexible" is used to indicate that the winding is flexible down to a radius of curvature in the order of eight to twenty-five times the cable diameter.

The winding should be constructed to retain its properties even when it is bent and when it is subjected to thermal stress during operation. It is vital that the layers retain their adhesion to each other in this context. The material properties of the layers are decisive here, particularly their elasticity and relative coefficients of thermal expansion. In a XLPE-cable, for instance, the insulating layer consists of cross-linked, low-density polyethylene, and the semiconducting layers consist of polyethylene with soot and metal particles mixed in. Changes in volume as a result of temperature fluctuations are completely absorbed as changes in radius in the cable and, thanks to the comparatively slight difference between the coefficients of thermal expansion in the layers in relation to the elasticity of these materials, the radial expansion can take place without the adhesion between the layers being lost.

The material combinations stated above should be considered only as examples. Other combinations fulfilling the conditions specified and also the condition of being semiconducting, i.e. having a conductivity within the range of $1-10^5$ ohm-cm, and being insulating respectively, i.e. with a conductivity less than 10^5 ohm-cm.

For example, the insulating layer may consist of a solid thermoplastic material such as low density polyethylene (LDPE), high density polyethylene (HDPE), polypropylene (PP), polybutylene (PB), polymethyl-pentene (PMP), cross-linked materials such as cross-linked polyethylene (XLPE), or rubber such as ethylene-propylene rubber (EPR) or silicone rubber.

The inner and outer semiconducting layers may be of the same basic material but with particles of conducting material such as soot or metal powder mixed in.

The mechanical properties of these materials, particularly their coefficients of thermal expansion, are affected relatively little by whether soot or metal powder is mixed in or not. The insulating layer and the semiconducting layers thus have substantially the same coefficients of thermal expansion.

Ethylene-vinyl-acetate copolymer/nitrile rubber, butylimp polyethylene, ethylene-acrylate-copolymers and ethylene-ethyl-acrylate copolymers may also constitute suitable polymers for the semiconducting layers.

Even when different types of material are used as base in the various layers, it is desirable for their coefficients of thermal expansion to be substantially the same. This is the case with the combination of the materials listed above.

5 The materials listed above have an elasticity which is sufficient to absorb minor differences between the coefficients of thermal expansion for the materials in the layers in the radial direction of the elasticity, so that no cracks or other damage appear, and so that the layers are not released from each other.

10 The conductivity of the two semiconducting layers is sufficient to substantially equalize the potential along each layer. At the same time, the conductivity is so small that the outer semiconducting layer has sufficient resistivity to contain the electrical field in the cable.

Thus, each of the two semiconducting layers essentially constitutes one equipotential surface, and the winding composed of these layers will substantially enclose the electrical field within it.

15 There is, of course, nothing to prevent one or more additional semiconducting layers being arranged in the insulating layer.

Brief description of the drawings

20 The invention will now be described in more detail with reference designations as in the accompanying drawings.

Figure 1 shows schematically a perspective view of a section diagonally through the stator of a rotating electric machine;

Figure 2 shows a cross section through a high-voltage cable in accordance with the present invention;

25 Figure 3 shows schematically a sector of a rotating electric machine;

Figure 4 shows a cross section through part of the sector shown in Fig. 3 where the cross section is marked by a rectangle.

Description of the invention

30 Figure 1 shows part of an electric machine in which the rotor has been removed to reveal more clearly how a stator 1 is arranged. The main parts of the stator 1 consist of a stator frame 2, a stator core 3 comprising stator teeth 4 and a

stator yoke 5. The stator also comprises a stator winding 6 in the form of a high-voltage cable, placed in a space 7 shaped like a bicycle chain, see Figure 3, formed between each individual stator tooth 4. In Figure 3 the stator winding 6 is only indicated by its electric conductors. As shown in Figure 1, the stator winding 6 forms a coil-end bundle 8 on each side of the stator 1. Figure 3 also reveals that the insulation of the high-voltage cable is stepped in several dimensions depending on its radial location in the stator 1. For the sake of simplicity only one coil-end bundle is shown in Figure 1 at each end of the stator.

In large conventional machines the stator frame 2 often consists of a welded steel plate construction. In large machines the stator core 3, also known as the laminated core, is normally made of 0.35 mm core sheet, divided into stacks having an axial length of approximately 50 mm and separated from each other by partitions forming ventilation ducts 5 mm wide. However, in the machine described the ventilation ducts have been eliminated. In large machines each laminated stack is formed by placing sheet metal segments 9, punched to a suitable size, together to form a first layer, each subsequent layer being laid cross-wise to form a complete laminated part of a stator core 3. The parts and partitions are held together by pressure brackets 10 which are pressed against pressure rings, fingers or segments, not shown. Only two pressure brackets are shown in Figure 1.

Figure 2 illustrates a cross section through a high-voltage cable 11 in accordance with the invention. The high-voltage cable 11 comprises a number of strand parts 12 made of copper (Cu), for instance, and having circular cross section. These strand parts 12 are arranged in the middle of the high-voltage cable 11. Around the strand parts 12 is a first semiconducting layer 13. Around the first semiconducting layer 13 is an insulating layer 14, e.g. XLPE insulation. Around the insulating layer 14 is a second semiconducting layer 15. The concept "high-voltage cable" in the present application thus does not comprise the outer protective sheath that normally surrounds a cable for power distribution. The high-voltage cable has a diameter within the interval 20-250 mm and a conducting area within the interval 80-3000 mm². In the figure showing the component forming the insulated conductor or cable, the three layers are such that they adhere to each

other even when the cable is bent. The shown cable is flexible and this property is retained throughout the service life of the cable.

Figure 3 shows schematically a radial sector of a machine with a sheet metal segment 9 of the stator 1 and a rotor pole 16 on the rotor 17 of the machine. It is also clear that the high-voltage cable 11 is arranged in the space 7 resembling a bicycle chain, formed between each stator tooth 4. Space 7 is shown in the figure in the shape of a bicycle chain, though as shown in Figure 4, according to one embodiment of the present invention, one side of the slot is entirely flat.

Figure 4 shows four cable parts 18 of the high-voltage cable 11, which parts are fitted into an asymmetric stator tooth slot 20 having an undulated side 21 in order to fit against the cable parts and a flat side 22. This shape of the stator tooth slots 20 results in triangular spaces 23 between each cable part 18. In each or in some of these spaces 23, tube members 24 are placed having been pre-shaped to correspond to the shape of space 23, though of a lesser dimension in order to permit easy insertion into the space 23. The term "tube member" designates in the following both the member's function as "cooling tube" and as a "fixing means".

The tube member 24 is inserted into the space 23 and a pressure medium is heated pressurising the tube member 24 which will soften and expand, its outer periphery assuming the shape of the restricting area of space 23 delimited by the cable parts second semiconducting layer 15 and the flat side 22 of the stator tooth slot 20, whereafter, maintaining a constant pressure, the warm pressure medium is substituted by a cold pressure medium filling the expanded tube member 24 and causing it to solidify and permanently assuming this expanded shape. It is possible to use the same pressure medium, though at different temperatures. In that case, the temperature of the warm pressure medium will be higher than the softening temperature of the tube member while the temperature of the cold pressure medium will keep below the softening temperature of the tube member. In order to prevent expansion of the free parts of the tube member, i.e. the parts situated outside the stator, these parts are provided with an expansion guard before the pressurisation of the cooling tube is started.

Each tube member 24 is made of a dielectric material, e.g. a polymer, preferably XLPE, in order to prevent electric contact with the plate of the stator tooth 4 or with the second semiconducting layer 15 of the cable parts 18.

During expansion the wall thickness of tube member 24 is reduced. The tube member 24 is allowed to expand until 50 % of its original wall thickness G remains. The wall thickness and other properties of the tube member are chosen in order to ensure that, after being expanded, the remaining wall thickness is sufficient to completely fill out the space between the outer periphery of the tube member and the second semiconducting layer 15 of the cable parts and the flat side 22 of the stator tooth slot respectively. The material of the tube member is determined with respect to factors like coefficient of thermal conductivity, coefficient of linear expansion as well as hot forming property.

Although the described embodiment relates to a triangular cable interspace, other forms of interspaces are possible, e.g. the cables may be arranged at a larger radial distance thereby forming a hour-glass-shaped interspace in which a pre-shaped cooling tube/fixing means of hour-glass shape may be arranged according to the present invention. It is also possible that the tube member prior to being expanded presents a different cross section than the space itself, e.g. an elliptic cross section, but that the tube member has a wall thickness allowing sufficient expansion.